



$p-n$ Junction

- ▶ 3.1 THERMAL EQUILIBRIUM CONDITION
- ▶ 3.2 DEPLETION REGION
- ▶ 3.3 DEPLETION CAPACITANCE
- ▶ 3.4 CURRENT-VOLTAGE CHARACTERISTICS
- ▶ 3.5 CHARGE STORAGE AND TRANSIENT BEHAVIOR
- ▶ 3.6 JUNCTION BREAKDOWN
- ▶ 3.7 HETEROJUNCTION
- ▶ SUMMARY

3.6.2 Avalanche Multiplication

- ❖ The avalanche multiplication process is illustrated in Fig. 22b.
- ❖ The $p-n$ junction, such as a p^+-n one-sided abrupt junction with a doping concentration of $N_D \cong 10^{17} \text{ cm}^{-3}$ or less, is under reverse bias.
- ❖ A thermally generated electron in the depletion region (designated by 1) gains kinetic energy from the electric field.

- ❖ If the field is sufficiently high, the electron can gain enough kinetic energy that on collision with an atom, it can break the lattice bonds, creating an electron-hole pair (2 and 2').
- ❖ The newly created electron and hole both acquire kinetic energy from the field and create additional electron-hole pairs (e.g., 3 and 3').
- ❖ These in turn continue the process, creating other electron-hole pairs.
- ❖ This process is therefore called avalanche multiplication.

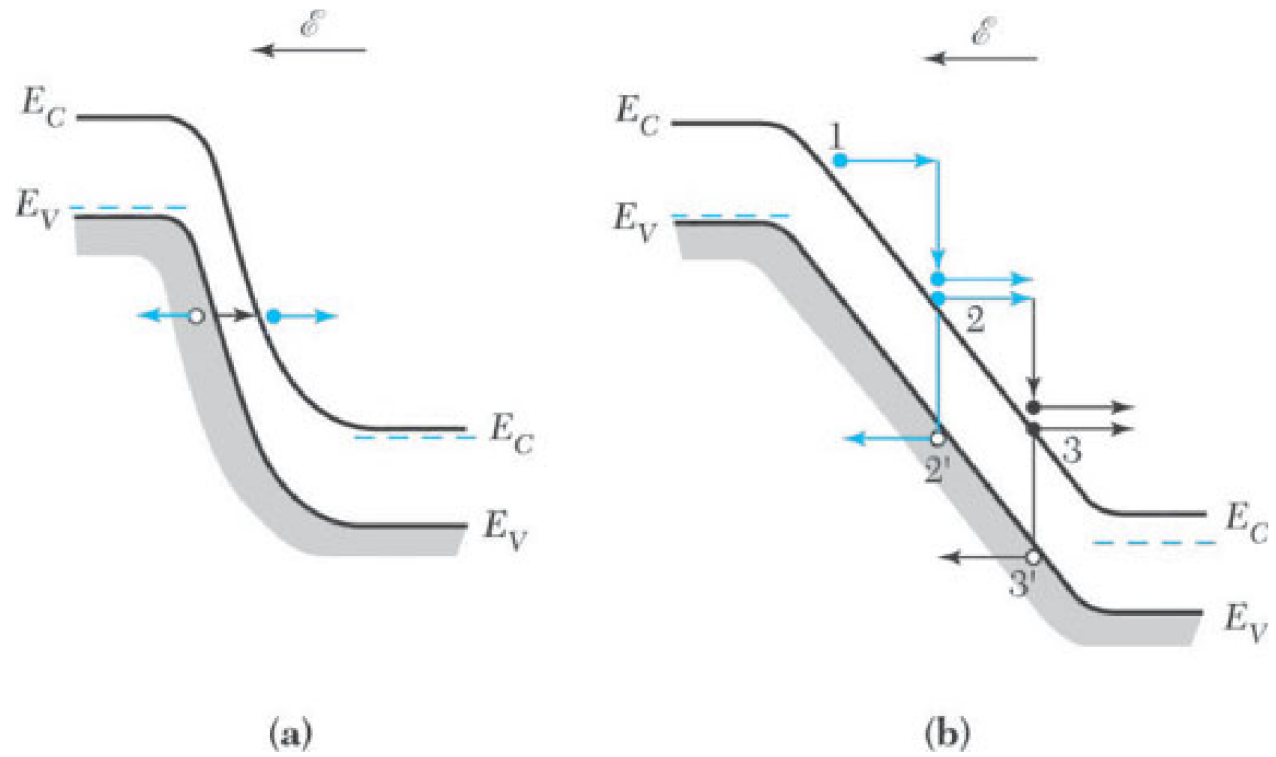


Fig. 22 Energy band diagrams under junction-breakdown conditions. (a) Tunneling effect. (b) Avalanche multiplication.

- ❖ To derive the breakdown condition, we assume that a current I_{no} is incident (وارد شدن) at the left-hand side of the depletion region of width W , as shown in Fig. 23.
- ❖ If the electric field in the depletion region is high enough to initiate (آغاز کردن) the avalanche multiplication process, the electron current I_n will increase with distance through the depletion region to reach a value $M_n I_{no}$ at W , where M_n , the multiplication factor, is defined as

$$M_n \equiv \frac{I_n(W)}{I_{no}}. \quad (81)$$

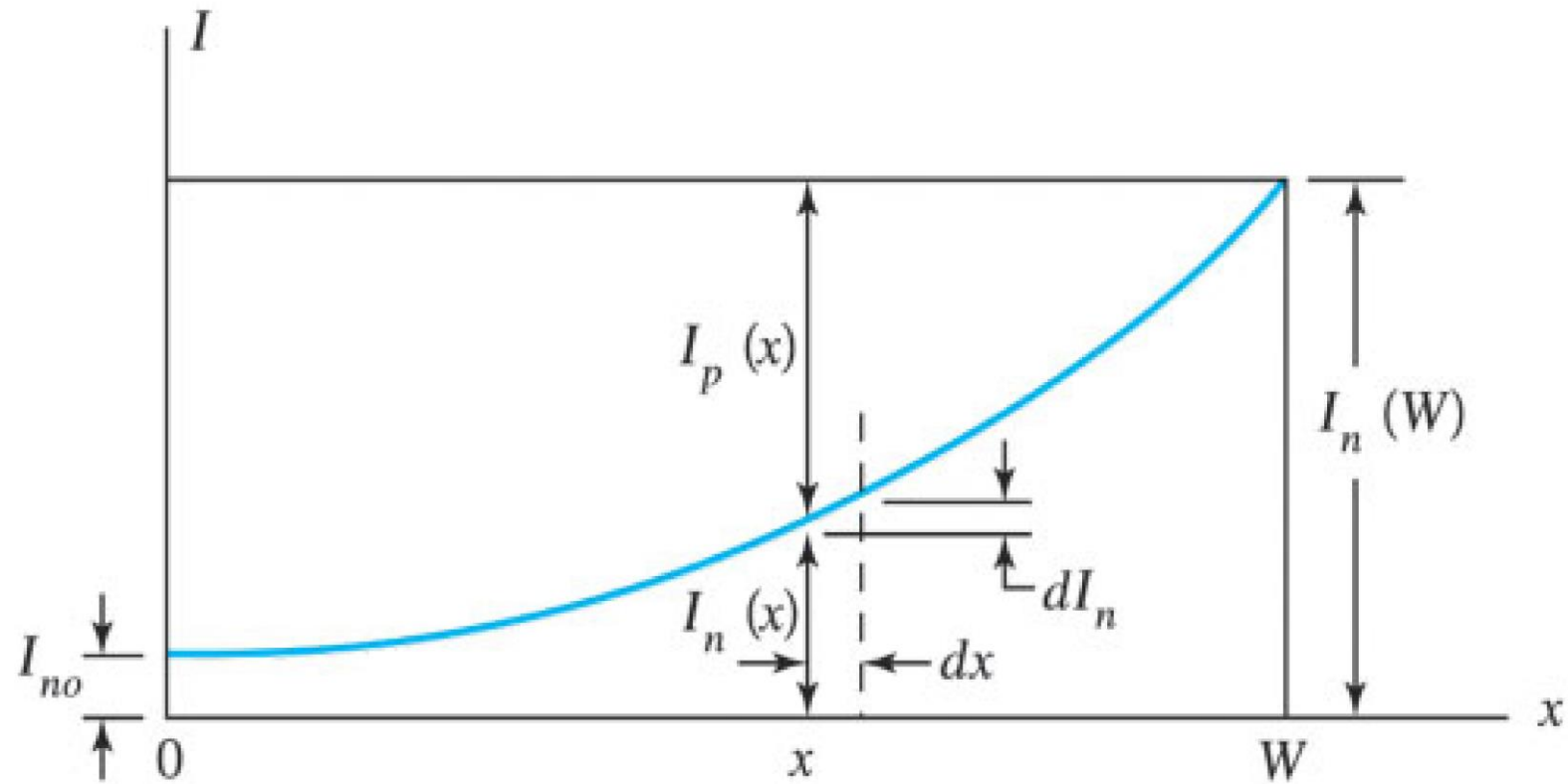


Fig. 23 Depletion region in a p - n junction with multiplication of an incident current.

❖ Similarly, the hole current I_p increases from $x = W$ to $x = 0$.

❖ The total current $I = (I_p + I_n)$ is constant at steady state.

❖ The incremental electron current at x equals the number of electron-hole pairs

generated per second in the distance dx :

افزایش جریان الکترونی با وجود تولید زوج الکترون حفره ها بخاطر این است که هر چه به سمت $x=W$ می رویم غلظت الکترونها هم رو به افزایش می گذارد چون به سمت ناحیه N حرکت می کنیم

$$\downarrow \quad d\left(\frac{I_n}{q}\right) = \left(\frac{I_n}{q}\right)(\alpha_n dx) + \left(\frac{I_p}{q}\right)(\alpha_p dx) \quad (82)$$

اثبات در اسلاید ۱۰

$$\frac{dI_n}{dx} + (\alpha_p - \alpha_n)I_n = \alpha_p I, \quad (82a)$$

❖ where α_n and α_p are the electron and hole ionization rates, respectively.

❖ If we use the simplified assumption that $\alpha_n = \alpha_p = \alpha$, the solution of Eq. 82a is

$$\frac{I_n(W) - I_n(0)}{I} = \int_0^W \alpha dx. \quad (83)$$

❖ From Eqs. 81 and 83, we have

اثبات در اسلاید بعدی

$$1 - \frac{1}{M_n} = \int_0^W \alpha dx. \quad (83a)$$

❖ The avalanche breakdown voltage is defined as the voltage at which M_n approaches infinity.

اثبات روابط ۸۲، ۸۲ا، ۸۳، ۸۳ا

$$dI_n = I_n \alpha_n dx + I_p \alpha_p dx$$

می‌توان نوشت:

یعنی نوعی تغییر در جریان الکترون برابری با تعداد زوج الکترون - حفره تولیدی در واحد زمان (ثانیه) در بازه طول dx

با تقسیم طرفین رابطه فوق بر dx رابطه ۸۲ به دست می‌آید ولی برای این آوردن رابطه ۸۲ا با توجه به اینکه $I = I_n + I_p$ ، $I_p = I - I_n$ خواهیم داشت:

$$dI_n = I_n \alpha_n dx + (I - I_n) \alpha_p dx$$

$$\rightarrow \frac{dI_n}{dx} = -I_n(\alpha_p - \alpha_n) + I \alpha_p$$

$$\rightarrow \frac{dI_n}{dx} + I_n(\alpha_p - \alpha_n) = I \alpha_p$$

با فرض: $\alpha_p = \alpha_n = \alpha$

$$\frac{dI_n}{dx} = I \alpha_p \rightarrow \frac{dI_n}{I} = \alpha dx \rightarrow \frac{1}{I} \int_{I_n(0)}^{I_n(w)} dI_n = \int_0^w \alpha dx$$

$$\rightarrow \frac{1}{I} (I_n(w) - I_n(0)) = \int_0^w \alpha dx$$

با توجه به اینکه $I_n(w) = I$ خواهد بود یعنی جریان کل در $x=w$ برابر جریان الکترونی در آن موقعیت بود و جریان حفره‌ای صفر است (از روی نمودار ۲۳ نیز آشکار است):

$$\frac{I - I_n(0)}{I} = \int_0^w \alpha dx \rightarrow 1 - \frac{I_n(0)}{I} = \int_0^w \alpha dx$$

صفتاً: $M_n = \frac{I_n(w)}{I_n(0)}$ و چون $I_n(w) = I$ پس $\frac{I_n(0)}{I} = \frac{1}{M_n}$ لذا:

$$1 - \frac{1}{M_n} = \int_0^w \alpha dx$$

❖ Hence, the breakdown condition is given by

$$\int_0^W \alpha dx = 1 . \quad (84)$$

❖ From both the breakdown condition described above and the field dependence of the ionization rates, we may calculate the critical field (i.e., the maximum electric field at breakdown) at which the avalanche process takes place.

شرط اول میدان بالا و شرط دوم رابطه ۸۴

↓ ❖ Using measured α_n and α_p (Fig. 27 in Chapter 2), the critical field E_c is calculated for silicon and gallium arsenide one-sided abrupt junctions and shown in Fig. 24 as functions of the impurity concentration of the substrate.

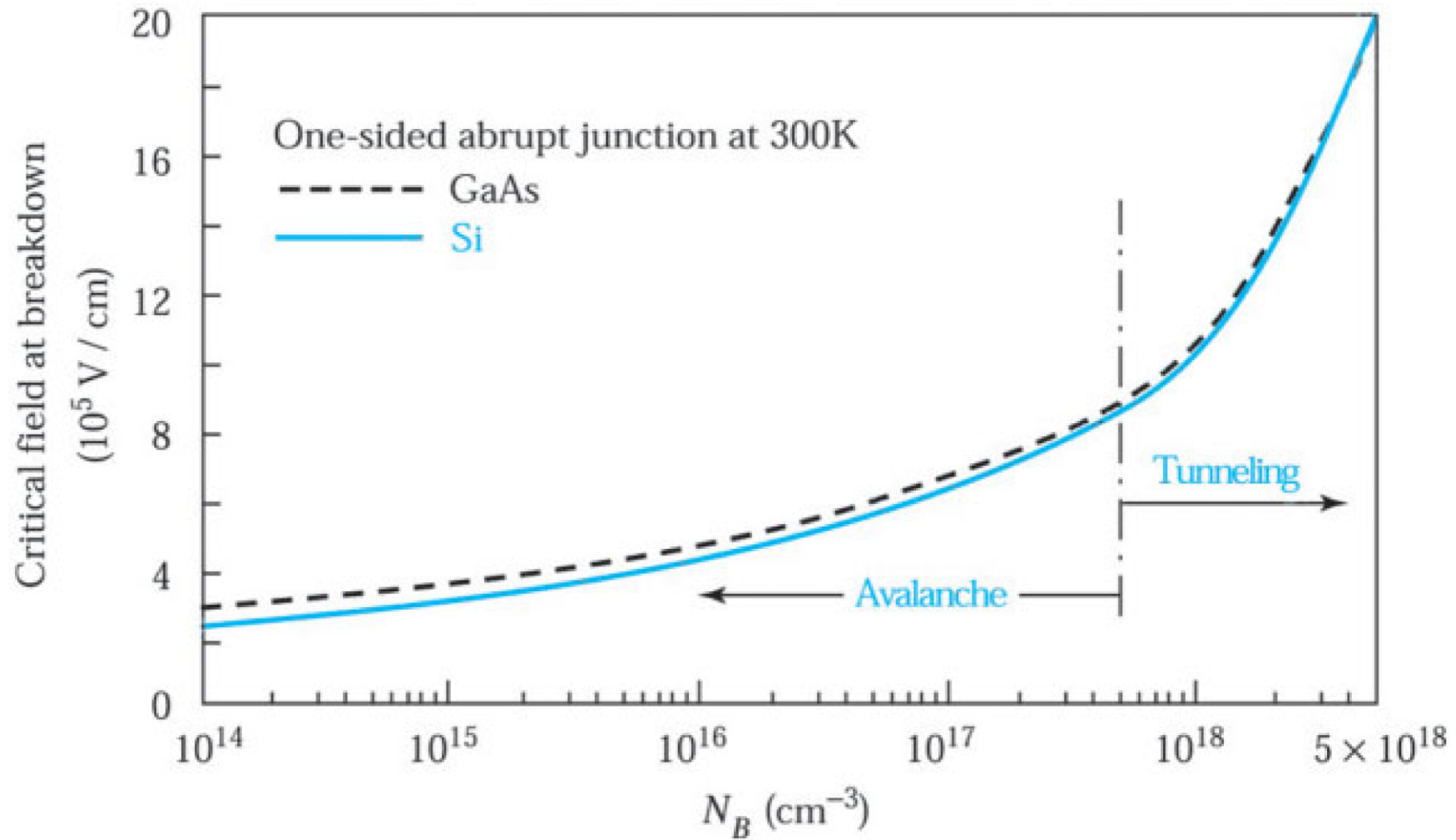


Fig. 24 Critical field at breakdown versus background doping for Si and GaAs one-sided abrupt junctions.⁵

- ❖ Also indicated is the critical field for the tunneling effect.
- ❖ It is evident that tunneling occurs only in semiconductors having high doping concentrations.
- ❖ With the critical field determined, we may calculate the breakdown voltages.
- ❖ As discussed previously, voltages in the depletion region are determined from the solution of Poisson's equation:

$$V_B (\text{breakdown voltage}) = \frac{\mathcal{E}_c W}{2} = \frac{\epsilon_s \mathcal{E}_c^2}{2q} (N_B)^{-1} \quad (85)$$

for one-sided abrupt junctions and

$$V_B = \frac{4\epsilon_c^{3/2}}{3} \left(\frac{2\epsilon_s}{q} \right)^{1/2} (a)^{-1/2} \quad \text{اثبات ۸۵ و ۸۶ در اسلاید بعدی} \quad (86)$$

for linearly graded junctions.

where N_B is the background doping of the lightly doped side, ϵ_s is the semiconductor permittivity, and a is the impurity gradient.

❖ The breakdown voltage, as a first-order approximation, varies as N_B^{-1} for abrupt junctions and as $a^{-1/2}$ for linearly graded junctions.

اثبات روابط ۸۵، ۸۶:

در حالت abrupt junction (بیوزین صلبه رابط ۱۹) داریم:

$$V_{bi} = \frac{1}{2} \epsilon_m W \quad (19)$$

همچنین در حالت فوق برای بیوزیک طرفه $p^+ - n$ نیز داریم: (رابطه ۲۷)

$$\epsilon_m = \frac{q N_B W}{\epsilon \epsilon_s} \quad (27) \rightarrow W = \frac{\epsilon_m \epsilon_s}{q N_B}$$

$$(19, 27) \Rightarrow V_{bi} = \frac{1}{2} \epsilon_c \frac{\epsilon_s \epsilon_m}{q N_B} = \frac{\epsilon_s \epsilon_c^2}{2q} (N_B)^{-1} \rightarrow (85)$$

و با فرض $\epsilon_m = \epsilon_c$

$$V_{bi} = V_B$$

ϵ_m میدان ماکزیم در این نوع بیوزات که در شکل V نیز آنرا دیدیم (اسدی بعدی)

و در حالت بیوز خطی (Linearly graded junction) داریم: (مطابق شکل ۹)

$$\epsilon_m = \frac{q a W^2}{12 \epsilon_s} \quad (29a)$$

$$V_{bi} = \frac{q a W^3}{12 \epsilon_s} \quad (30)$$

$$(29a) \rightarrow W^2 = \frac{12 \epsilon_s \epsilon_m}{q a}$$

مثابه حالت قبل با فرض $\epsilon_m = \epsilon_c$ و $V_{bi} = V_B$

$$W = \left(\frac{12 \epsilon_s \epsilon_c}{q a} \right)^{\frac{1}{2}} *$$

$$(*, 30) \Rightarrow V_B = \frac{q a}{12 \epsilon_s} \left(\frac{12 \epsilon_s \epsilon_c}{q a} \right)^{\frac{3}{2}} = \frac{12 \epsilon_c^{\frac{3}{2}}}{3} \left(\frac{12 \epsilon_s}{q} \right)^{\frac{1}{2}} (a)^{-\frac{1}{2}}$$

بنظر می رسد در رابطه ۱۹ بدلیل اینکه ولتاژ معکوس اعمال می شود باید بجای V_{bi} کمیت $V - V_{bi}$ را قرار دهیم و در واقع V_B که پتانسیل شکست است، مقدار پتانسیل منتج است. همین بحث در مورد میدان الکتریکی نیز صادق است.

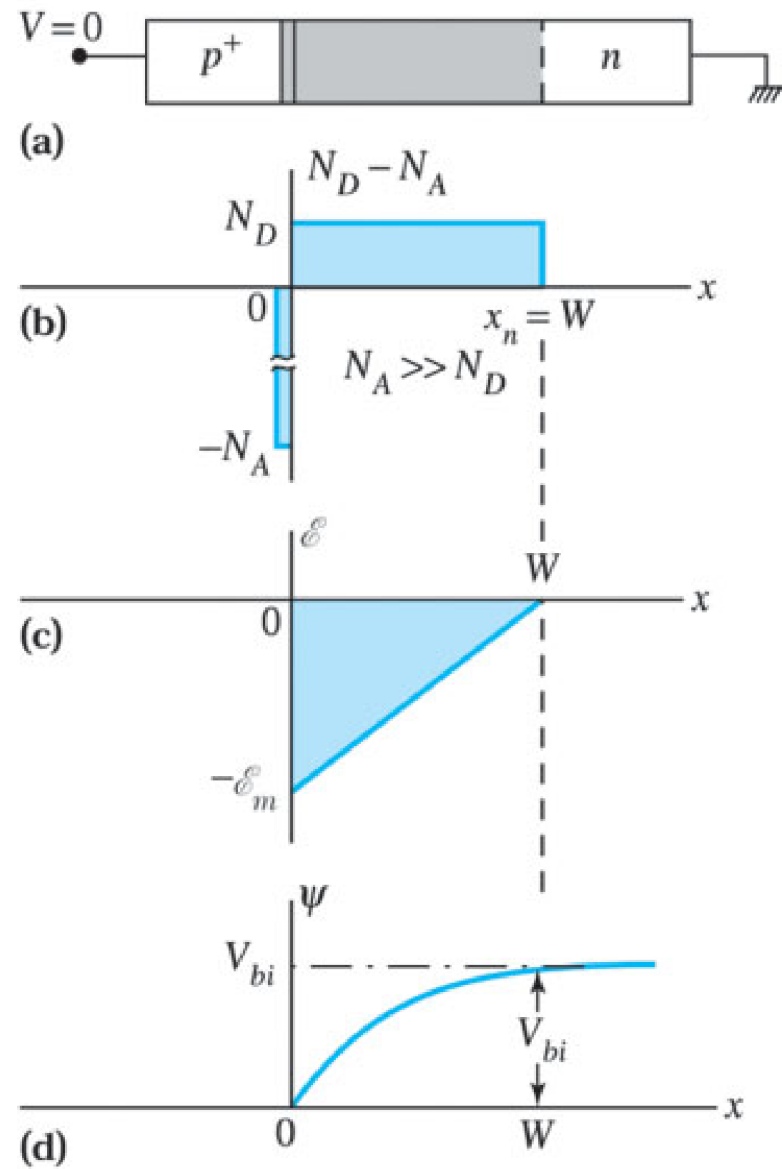


Fig. 7 (a) One-sided abrupt junction (with $N_A \gg N_D$) in thermal equilibrium. (b) Space charge distribution. (c) Electric-field distribution. (d) Potential distribution with distance, where V_{bi} is the built-in potential.

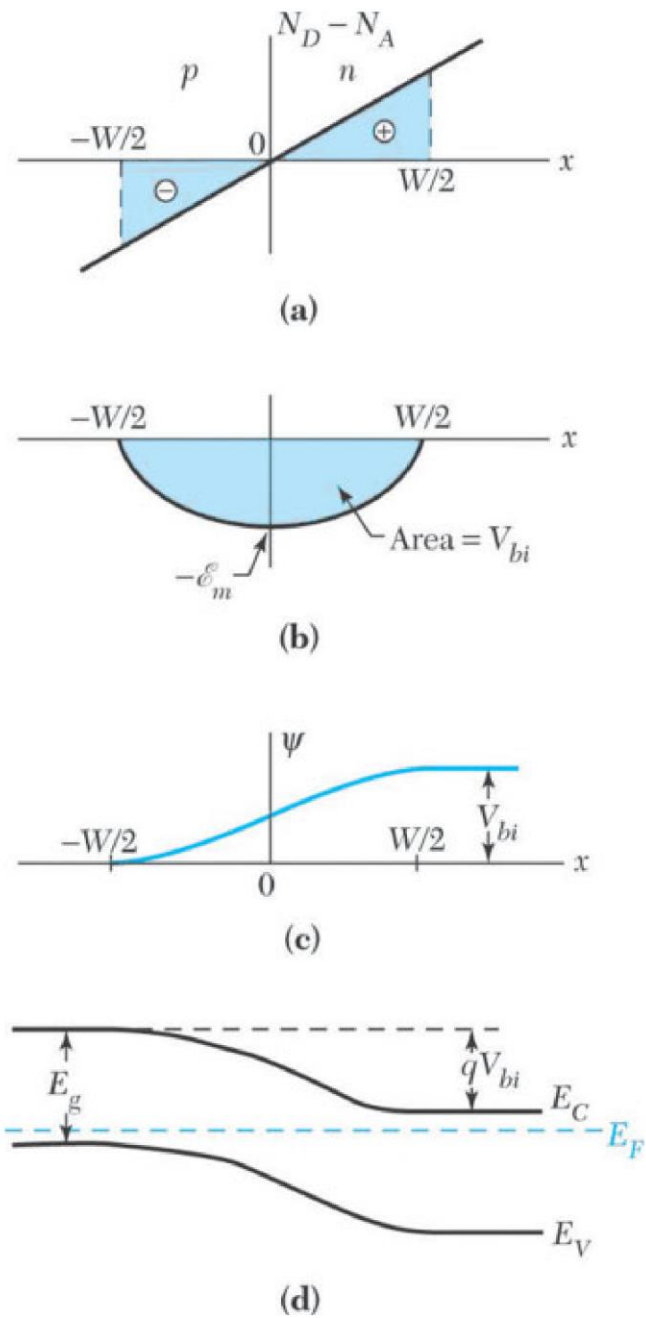


Fig. 9 Linearly graded junction in thermal equilibrium. (a) Impurity distribution. (b) Electric field distribution. (c) Potential distribution. (d) Energy band diagram.

- ❖ Figure 25 shows the calculated avalanche breakdown voltages for silicon and gallium arsenide junctions.
- ❖ The dash-dot line (to the right) at high dopings or high-impurity gradients indicates the onset of the tunneling effect.
- ❖ Gallium arsenide has higher breakdown voltages than silicon for a given N_B or a , mainly because of its larger bandgap.
- ❖ The larger the bandgap, the larger the critical field must be for sufficient kinetic energy to be gained between collisions.

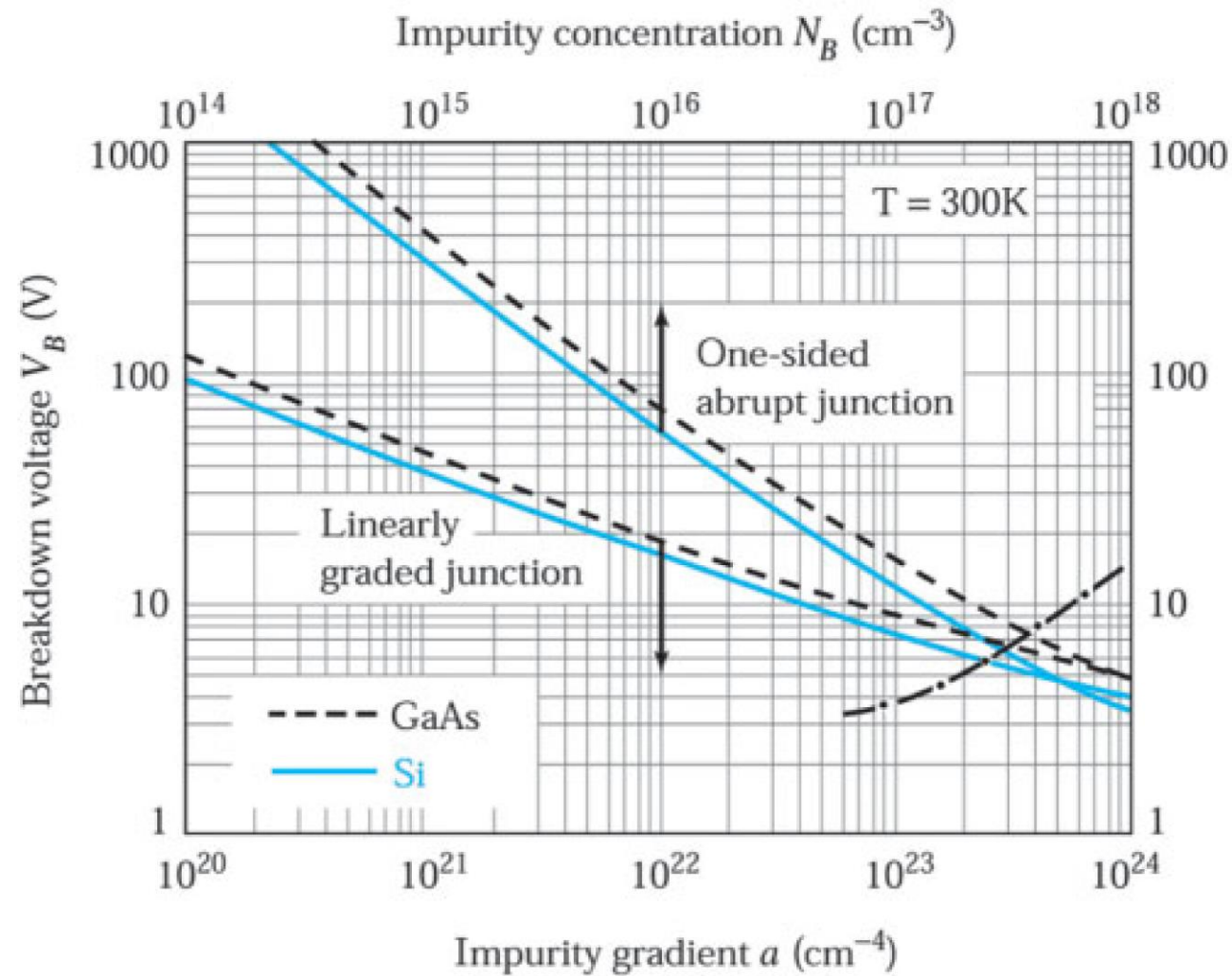


Fig. 25 Avalanche breakdown voltage versus impurity concentration for a one-sided abrupt junction and avalanche breakdown voltage versus impurity gradient for a linearly graded junction in Si and GaAs. Dash-dot line indicates the onset of the tunneling mechanism.⁵

❖ As Eqs. 85 and 86 demonstrate, the larger critical field, in turn, gives rise to higher
↓ breakdown voltage.

EXAMPLE 8

Calculate the breakdown voltage for a Si one-sided p^+n abrupt junction with $N_D = 5 \times 10^{16} \text{ cm}^{-3}$.

SOLUTION From Fig. 24, we see that the critical field at breakdown for a Si one-sided
↓ abrupt junction is about $5.7 \times 10^5 \text{ V/cm}$. Then from Eq. 85, we obtain...