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# Chap.12

## Light Sources

Photonics and Lasers An Introduction, Richard S. Quimby,

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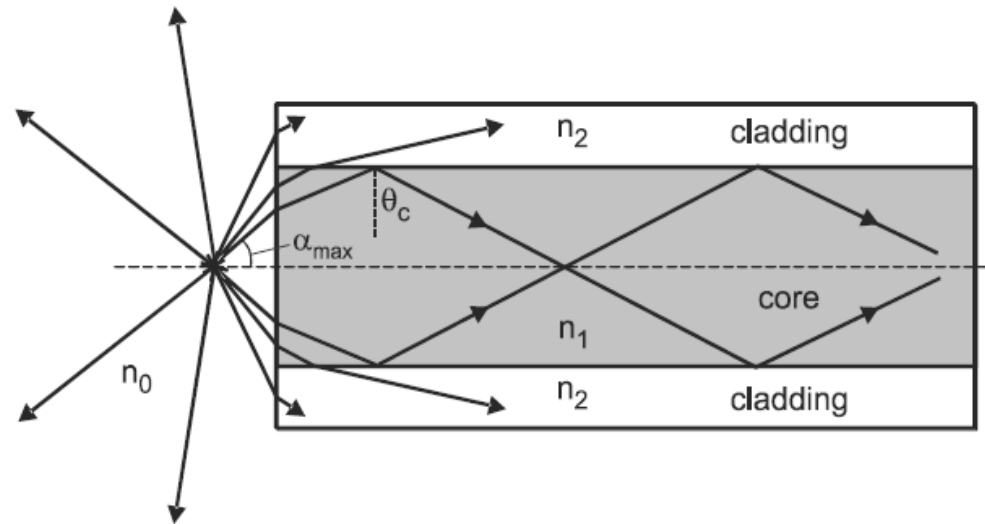
# Introduction

- We saw in previous chapters how light propagates in a **waveguide**.
- And how the light can be **generated** by an **LED** or **laser diode**.
- A related issue is the efficiency which light can be coupled from a **light source** into a **waveguide**.
- In this chapter we examine this **efficiency** for sources with **different degrees of directionality**.
- It will be seen that the **coupling efficiency** is greater for **more directional sources**.

# 12.1. Point Source

- Consider first **isotropic** emission, in which light appears to emanate from **a point**.
- We like to calculate the **fraction of emitted power** that is collected by **an optical fiber**, as illustrated in **Fig. 12-1**.

**Figure 12-1** Light rays from a point source making a sufficiently **small angle** with the fiber axis are coupled into the **fiber core** (shaded area).



# 12.1. Point Source -2

- If a **point source** emitting a total power  **$P_s$**  is embedded in a uniform medium of refractive index  **$n_0$**  outside the fiber.
- It will radiate light equally into all  **$4\pi$**  steradians of solid angle, with an emitted power per unit solid angle of  **$P_s/4\pi$** .
- However, only those rays making an **angle  $\alpha < \alpha_{max}$**  with the fiber axis will be trapped by the fiber, where:

$$\sin \alpha_{max} = NA/n_0 .$$

- **NA** is the numerical aperture of the fiber.

# 12.1. Point Source-3

We know that light will be trapped is:

$$\begin{aligned}\Omega &= 2\pi(1 - \cos \alpha_{\max}) && (12-1) \\ &= 2\pi(1 - \sqrt{1 - \sin^2 \alpha_{\max}}) \\ &= 2\pi(1 - \sqrt{1 - (\text{NA}/n_0)^2}) \\ &\approx 2\pi \frac{1}{2} \left(\frac{\text{NA}}{n_0}\right)^2 = \pi \frac{\text{NA}^2}{n_0^2}\end{aligned}$$

➤ Where in the last step the expansion

$$(1 + x)^n \approx 1 + nx$$

➤ Has been used, along with the approximation ( good for most optical fibers)  $\text{NA}^2 \ll 1$  .

## 12.1. Point Source-4

➤ Since the light is distributed **uniformly** with angle, the power coupled into the fiber is given by

$$P_{\text{in}} = \left( \frac{\Omega}{4\pi} \right) P_s \quad (12-2)$$

➤ Which leads to the coupling efficiency

$$\eta_c \equiv \frac{P_{\text{in}}}{P_s} = \frac{\Omega}{4\pi} = \frac{NA^2}{n_0^2} \quad (12-3)$$

➤ This result shows that **higher numerical aperture** fibers accept **a larger fraction of the emitted light** from **a point source**.

## 12.2. Lambertian Source

- Many practical light source such as the LED are best treated as **extended sources**, in which light is emitted over some **surface area** .
- The emitting surface is characterized by a **brightness**.
- Defined as the power emitted **per unit solid angle**, per **unit surface area**.
- This brightness is found in many cases to vary with direction as :

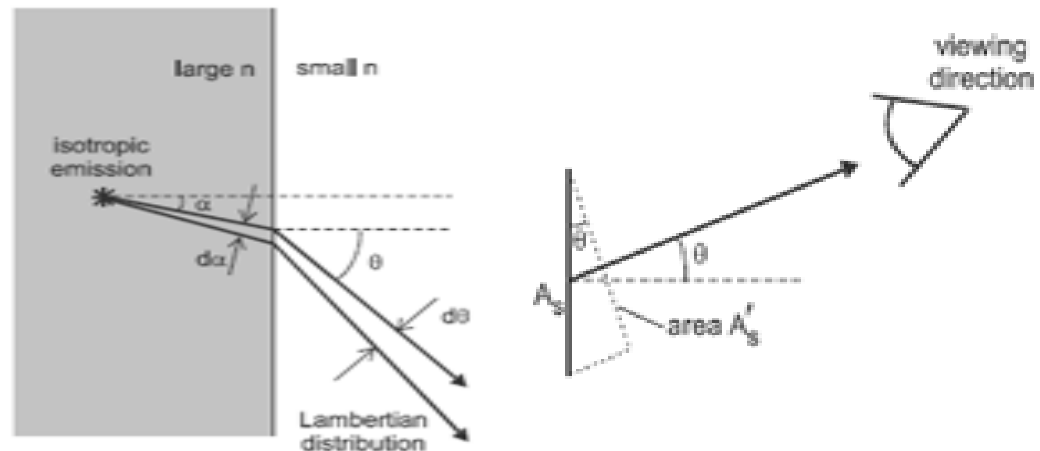
$$B(\theta) = B(0) \cos \theta \quad (\text{Lambert's law}) \quad (12-4)$$

- Where  $\theta$  is the angle to the surface normal.



## 12.2. Lambertian Source-2

- A light-emitting surface with an angular distribution given by Eq. (12-4) is known as a **Lambertian source**.
- The dependence to  **$\cos\theta$**  can be understood by referring to **Fig. 12.2**.



**Figure 12-2 (a)** Light emitted isotropically inside a high-index medium becomes distributed according to Lambert's law after refraction at a boundary.

**(b)** when viewed off-axis, light from an emitting surface appears to come from the projected area.

## 12.2. Lambertian Source-3

- Which shows light being generated inside a **high refractive index material** and emitted into **air**.
- Inside the material, light is emitted **isotropically**, and equal  **$d\Omega = 2\pi \sin \theta d\theta$**  of light is radiated into each differential solid angle:
  - .
- Because of refraction at the boundary, however, the  **$d\Omega = 2\pi \sin \theta d\theta$**  corresponding solid angle on the air side, becomes proportionately larger as  $\theta$  increases.
- Since the  **$\theta$**  same optical power is spread out over a larger solid angle as  $\theta$  increases, the **brightness** decreases.

## 12.2. Lambertian Source-4

➤ This argument can be made quantitative by using **Snell's law** to relate the **two solid angles**.

➤ The resulting brightness (including **Fresnel reflection** losses at the boundary) is:

$$B(\theta) = \frac{P_s}{\pi A_s n(n+1)^2} \cos \theta \quad (12-5)$$

➤ Where **P<sub>s</sub>** is the total power emitted inside the material, and **A<sub>s</sub>** is the **emission surface area**.

➤ assumed in deriving this that the index of refraction **n** is large ( $n > 2.5$ ), which is valid for most semiconductors.

## 12.2. Lambertian Source-5

- An alternative view of **Lamber's law** is to define an "apparent brightness"  $B_{\text{eff}}$  as the power per solid angle emitted in a certain direction, divided by the projected area of the surface.
- From **fig.12-2b**, this projected area is  $A'_s = A_s \cos \theta$ , so the apparent brightness is:

$$B_{\text{eff}} = \frac{\Delta P}{A'_s \Delta \Omega} = \frac{\Delta P}{A_s \Delta \Omega \cos \theta} = \frac{B(\theta)}{\cos \theta} \quad (12-6)$$

- If  $B_{\text{eff}}$  is independent of  $\theta$ , then  $B(\theta) \propto \cos \theta$ , which is **Lamber's law**.

## 12.2. Lambertian Source-6

- We can say, then, that a **Lambertian surface** is **one** for which the apparent **brightness is independent of viewing angle**.
- To determine coupling efficiency into a fiber, we first calculate the total power  $P_0$  emitted from the **Lambertian surface**.
- Integrating Eq.(12-4) over one hemisphere, we have :

$$B(\theta) = B(0) \cos \theta \quad (\text{Lambert's law}) \quad (12-4)$$

$$P_0 = A_s \int_0^{\pi/2} B(\theta) d\Omega \quad (12-7)$$

$$= A_s \int_0^{\pi/2} [B(0) \cos \theta][2\pi \sin \theta d\theta]$$

$$= 2\pi A_s B(0) \int_0^{\pi/2} \cos \theta \sin \theta d\theta$$

## 12.2. Lambertian Source-7

- Using the substitution  $u = \sin \theta$ ,  $du = \cos \theta d\theta$ , this can be evaluated as :

$$P_0 = 2\pi A_s B(0) \int_0^1 u du \quad (12-8)$$

$$= 2\pi A_s B(0) \frac{1}{2} u^2 \Big|_0^1$$

$$= \pi A_s B(0)$$

- Combining this with Eq. (12-5) for  $\theta = 0$  gives:

$$B(\theta) = \frac{P_s}{\pi A_s n(n+1)^2} \cos \theta \quad (12-5)$$

$$P_0 \simeq \frac{P_s}{n(n+1)^2} \quad (12-9)$$

## 12.2. Lambertian Source-8

- The ratio  $P_0/P_s$  corresponds to the LED external efficiency  $\eta_{ext}$  defined in Eq. (11-15).

$$\eta_{ext} = \frac{\Omega}{4\pi} T$$

- for GaAs ( $n=3.6$ ), Eq. (12-9) gives  $\eta_{ext} \approx 0.013$ .

$$P_0 \approx \frac{P_s}{n(n+1)^2} \quad (12-9)$$

- The power  $P_{in}$  coupled into the fiber is calculated in the same way as the total power, except that the upper limit on  $\theta$  is  $\sin \alpha_{max}$  rather than  $\pi/2$ . the upper limit on  $u$  in Eq. (12-8) is then  $\sin \alpha_{max}$  rather than 1, giving:

$$P_0 = 2\pi A_s B(0) \int_0^{\sin \alpha_{max}} u \, du \quad (12-8)$$

$$= 2\pi A_s B(0) \frac{1}{2} u^2 \Big|_0^{\sin \alpha_{max}}$$

$$= \pi A_s B(0) \sin^2 \alpha_{max}$$

## 12.2. Lambertian Source-9

$$\text{➤ } P_{\text{in}} = \pi A_s B(0) \sin^2 \alpha_{\text{max}} \quad (12-10)$$

$$\begin{aligned} &= P_0 \sin^2 \alpha_{\text{max}} \\ \eta_c &= \frac{P_{\text{in}}}{P_0} = \sin^2 \alpha_{\text{max}} = \left( \frac{\text{NA}}{n_0} \right)^2 \text{ efficiency for Lambertian source } (12-11) \end{aligned}$$

➤ This efficiency is the same as for a **point source**, except that it is **four times higher**.

➤ The difference comes from the more directional emission of the Lambertian source.

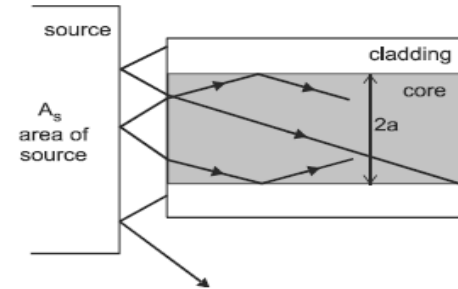
➤ With a greater fraction of the emitted light lying within the **angular acceptance range** of the fiber.

➤ For an extended source like an **LED**, the **coupling efficiency** also depends on the **size of the emitting area** compared with the core area of the optical fiber.



## 12.2. Lambertian Source-10

- As seen **fig.12-3**:



**Figure 12-3** Light striking the fiber outside the core area is not coupled, regardless of angle. This decreases the coupling efficiency when the emission area is greater than the fiber core area.

- light that is emitted outside of the core area **will not** be accepted by the fiber, regardless of emission angle.

## 12.2. Lambertian Source-11

➤ Only the fraction  $\pi a^2 / A_s$  will be accepted by the fiber if  $\pi a^2 < A_s$ .

➤ In this case, the coupling efficiency will be

$$\eta_c = \frac{\pi a^2}{A_s} \left( \frac{\text{NA}}{n_0} \right)^2 \quad (\text{coupling efficiency when } \pi a^2 < A_s) \quad (12-12)$$

➤ When  $\pi a^2 > A_s$ , the coupling efficiency depends only on emission angle, and Eq. (12-11) applies.

➤ **Edge-emitting LEDs** have a smaller emission area, making them **more efficient** for coupling into an optical fiber.

# Example 12.1

❖ A GaAs LED with a square emitting area of side 0.2 mm emits light through air into an optical fiber with core index 1.5, fractional index difference  $\Delta = 0.008$ , and core diameter 50  $\mu\text{m}$ . Determine (a) the coupling efficiency, and (b) total efficiency with which light generated inside the LED material is coupling into the fiber.

□ Solution:

(a) the numerical aperture is given by Eq. (4-5) as:

$$\text{NA} \simeq n\sqrt{2\Delta} = (1.5)\sqrt{2(0.008)} = 0.190$$

# Example-12.1-cont

✓ And the ratio of areas is:

$$\frac{\pi a^2}{A_s} = \frac{\pi(25 \times 10^{-6})^2}{(2 \times 10^{-4})^2} = 0.049$$

✓ Eq. (12-12) then gives:

$$\eta_c = \frac{\pi a^2}{A_s} \left( \frac{NA}{n_0} \right)^2$$

$$\eta_c = (0.049)(0.19)^2 = 1.77 \times 10^{-3}$$

(b) Using Eq. (12-9),

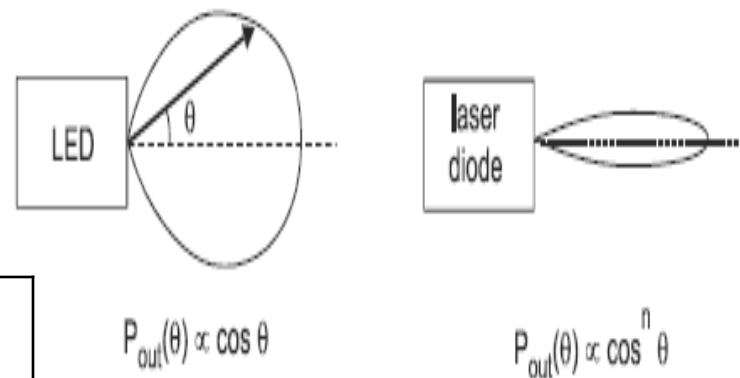
$$\frac{P_0}{P_s} = \frac{1}{n(n+1)^2} = \frac{1}{3.6(4.6)^2} = 0.013$$

The **total efficiency** is then:

$$\eta_{\text{tot}} = \frac{P_{\text{in}}}{P_s} = (0.013)(1.77 \times 10^{-3}) = 2.32 \times 10^{-5}$$

## 12.3. Laser source

- In the previous section, we saw that light obeying **Lamber's law** is coupled more efficiently into an optical fiber than light from a point source.
- Due to increased directionality in the **angular distribution**.
- We would expect laser light to be even more efficiently coupled, due to its high degree of directionality (see fig. 11-10).



**Figure 11-10** the angular distribution pattern is much more directional for a laser than for an LED.

## 12.3. Laser source-2

➤ To make a quantitative estimate of this improved coupling efficiency, the angular variation of a **laser's brightness** is taken to be:  $B(\theta) = B(0)\cos^m \theta$  (12-13)

➤ Where **m** is large, and not necessarily an integer.

➤ Although **this is not** the actual angular distribution for a laser,

➤ It can be a close approximation when the proper value of **m** is chosen, and it makes the calculations simpler.

➤ As for the **Lambertian emitter**, we first calculate the total power emitted,

$$P_0 = A_s \int_0^{\pi/2} B(0) \cos^m \theta \, 2\pi \sin \theta \, d\theta \quad (12-14)$$

$$= 2\pi A_s B(0) \int_0^{\pi/2} \cos^m \theta \sin \theta \, d\theta$$

## 12.3. Laser source-3

- Which can be valuated using the substitution  
 $u = \cos \theta, du = -\sin \theta d\theta$

As:

$$\begin{aligned}
 P_0 &= 2\pi A_s B(0) \int_0^1 u^m du && (12-15) \\
 &= 2\pi A_s B(0) \left[ \frac{u^{m+1}}{m+1} \right]_0^1 \\
 &= \frac{2\pi}{m+1} A_s B(0)
 \end{aligned}$$

- The power coupled into the fiber is determined in the same way, except that the upper limit on  $\theta$  is  $\alpha_{\max}$ , which leads to a lower limit on  $u$ .

- The power into the fiber is then

$$u_{\min} = \cos \alpha_{\max} = \sqrt{1 - \sin^2 \alpha_{\max}} = \sqrt{1 - (NA/n_0)^2}$$

$$P_{\text{in}} = \frac{2\pi}{m+1} A_s B(0) (1 - u_{\min}^{m+1}) \quad (12-16)$$

$$= \frac{2\pi}{m+1} A_s B(0) \left[ 1 - \left( 1 - \frac{NA^2}{n_0^2} \right)^{(m+1)/2} \right]$$

## 12.3. Laser source-4

➤ Which corresponds to a **coupling efficiency**:

$$\eta_c = \frac{P_{in}}{P_0} = 1 - \left(1 - \frac{NA^2}{n_0^2}\right)^{(m+1)/2} \quad (12-17)$$

➤ For small **NA** and **m** not too large, the binomial expansion  $(1 + x)^n \approx 1 + nx$  can be used to obtain the simplified result

$$\eta_c \simeq \frac{m+1}{2} \left(\frac{NA}{n_0}\right)^2 \quad (\text{laser coupling efficiency}) \quad (12-18)$$

❖ Equ.(12-18) is obviously not true for arbitrarily **large m**.



## Example 12.2

- ❖ A laser beam has an angular distribution with a full width at half maximum (FWHM) of  $20^\circ$ . Determine the value of  $m$  for this distribution, and calculate the coupling efficiency into a large core area optical fiber with  $NA = 0.22$ .

□ Solution:

The half width is  $10^\circ$ , so  $m$  is found from  $\frac{1}{2} = \cos^m 10^\circ$

Taking the natural log of both sides yields

$$\ln(0.5) = m \ln(\cos 10^\circ)$$

so

# Example -12.2-cont

$$m = \frac{\ln(0.5)}{\ln(\cos 10^\circ)} = 45.3$$

putting this into the approximate expression Eq. (12-18)

gives the result  $\eta_c \simeq \frac{m+1}{2} \left(\frac{NA}{n_0}\right)^2$  (laser coupling efficiency) (12-18)

$$\eta_c \simeq \frac{46.3}{2} (0.22)^2 = 1.12$$

Which is clearly not exact since  $\eta_c$  must be  $< 1$ . To get an accurate result here, it is necessary to use Eq. (12-7):

$$\eta_c = \frac{P_{in}}{P_0} = 1 - \left(1 - \frac{NA^2}{n_0^2}\right)^{(m+1)/2} \quad (12-17)$$

$$\eta_c = 1 - [1 - (0.22)^2]^{46.3/2} = 0.683$$

This efficiency is, as expected, must higher than that for an LED.

# Thank you for your attention

